Advertorial: Witteveen+Bos

Within the Netherlands, there are hundreds of movable bridges located throughout the entire country. These bridges are owned be several instances, like Rijkswaterstaat, ProRail, provinces, municipalities, but also water boards. These bridges should be considered as a machine with large, moving parts and therefore they can be assessed by means of the Machinery Directive (2006/42/EG). The main goal of this directive is to establish that these machines comply with the so-called essential health and safety requirements. In other words, the movable bridges in our country need to be safe.

Risk assessment identified, quantified and then reduced

In order to determine what 'safe' actually means, it is required by the Machinery Directive to perform a risk assessment movable bridges. By following a structured analysis the present risks are to be

or mitigated by taking adequate measures. A well-known method for performing risk assessment on machinery is described by ISO 12100. In the end, one will find a list of risks which need to be reduced.

Figure 1. Example of a movable bridge (Schinkelbruggen, Amsterdam).

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The first step in reducing risks is to alter the design, in order that either the hazard is removed or the risk has vanished. However, in many cases this step cannot be executed due to e.g. design specifications. The second step is to look for mechanical solutions, which prevent a person from entering hazardous areas, such as physical barriers and guards. Though, there are numerous situations in which these types of solutions do not suffice. For example, if maintenance is required, one will actually need to enter hazardous areas. Then, the solution for risk reduction can be yield by functional safety.

Functional safety in machinery usually means systems that safely monitor and, when necessary, override the machine applications to ensure safe operation. This means that a safety-related system implements the required safety functions by detecting hazardous conditions and bringing operation to a safe state, by ensuring that a desired action, e.g. safe stopping, takes place.

Generally, safety chains are designed in order to obtain the input ('sensor'), process this input by a control system ('logic') and perform an action on the machine ('actuator').

The way safe stopping actually needs to be realized is a matter of choice and standards. The standards for electronic safety systems are formally designated by both ISO 13849-1 for Performance Level (PL) and IEC 62061 for Safety Integrity Level (SIL).

In this article, the standard for SIL and its application on designing movable bridges is discussed, since the method of SIL is commonly used by Witteveen+Bos in projects on movable bridges.

(SIL)

IEC 62061 is the standard for designing electrical safety systems. It includes recommendations for the design, integration and validation of safety-related electrical, electronic and programmable electronic control systems for machinery. This standard also covers the entire safety chain, e.g. sensor-logic-actuator. As long as the entire safety function fulfils the defined requirements, individual sub-systems need not be certified.

The standard defines how to determine both the required and achieved Safety Functional safety

Functional safety

reliability of safety functions. Four SIL levels are possible: 1, 2, 3, and 4. 'SIL 4' is the highest level of safety integrity and 'SIL 1' the lowest. In the field of machinery (and thus movable bridges), only levels 1-3 are used.

Table 1. Overview of safety integrity levels

Figure 2. Example of a subsystem for a safety chain

Dangerous failure mon cause failure (CCF), for which a

In IEC 62061, a safety integrity requirement is expressed as a target failure value Safety Integrity Level for the probability of dangerous failure
per hour, PFH₁₂ as shown in table 1. A dangerous failure is to be considered as a situation where a malfunction of the system will lead to a dangerous situation (like unexpected movements of the machine).

> Additionally, there exist threshold values (per hour) for systems that do not contain sufficient diagnostic coverage (e.g. automatic diagnostic tests on proper component operation). This coverage DC can be expressed as the ratio between detected dangerous hardware

$$
DC = \frac{\Sigma \lambda_{DD}}{\Sigma \lambda_{D,total}}
$$

failures, $\sum \lambda_{\rm np}$, and the total of dangerous hardware failures $\sum \lambda_{\text{D,total}}$:

Determination of the value of PFH_{ro} depends of the design of the safety chain and choice of components and can be quite complicated. An example is given below, where a system is considered with single fault tolerance (i.e. redundant architecture) and without a diagnostic

Diagnosis
As can be derived from the analysis on architectural constraints, the other approach for achieving safety integrity is to design a 'smart' system. Such a system contains several diagnostic functions in which dangerous failures are either early detected or will lead directly lead to a

Architectural con-

To realize a system which vields a suffi-

cient integrity on safety, there are gene-

rally two approaches. The first approach

is to consider hardware fault tolerance,

by designing a system using a redundant

architecture (e.g. the previously men-

tioned subsystem). Though, there are

limits on what can be achieved on SIL,

by considering table 2, due to the lack of

where T, is the proof test interval or life-

time (smallest), β is the susceptibility to

common cause failures and λ is the fai-

single fault will lead to a failure by both

For such an architecture, the probability of dangerous failure of the subsystem is:

 $\lambda = (1-\beta^2)\lambda_1\lambda_2T_1 + \beta/2(\lambda_1+\lambda_2)$

straints

diagnosis.

lure rate.

channels.

 $PFH_n = \lambda \times 1$ h,

$$
SFF = \frac{\Sigma \lambda_{\rm S} + \Sigma \lambda_{\rm DD}}{\Sigma \lambda_{\rm S} + \Sigma \lambda_{\rm D}}
$$

